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## Complementary CC Amplifier

Figure 1 shows a complementary common-collector stage. This is commonly used as the final output stage in op amps and audio power amplifiers. Compared to a non-complementary CC amplifier, it can supply large positive and negative load currents with low power dissipation in the absence of a signal. The npn BJT supplies positive load current while the pnp BJT supplies negative load current.



Figure 1: Complementary common-collector amplifier.

Let us first examine the performance of the circuit with  $V_B = 0$ . For  $v_I = 0$ , both transistors are cut off. In order to obtain a positive output voltage,  $v_I$  must be increased until  $Q_1$  turns on. Denote the turn-on voltage for  $Q_1$  by  $V_{\gamma}$ . Similarly, denote the turn-on voltage for  $Q_2$  by  $-V_{\gamma}$ . When  $-V_{\gamma} < v_I < V_{\gamma}$ , both transistors are off and there is very little output voltage. For  $v_I > V_{\gamma}$ ,  $Q_1$  turns on and  $v_O$  goes positive. For  $v_I < -V_{\gamma}$ ,  $Q_2$  turns on and  $v_O$  goes negative. The plot of  $v_O$  versus  $v_I$  would resemble curve a in Fig. 2. A sine wave applied to the circuit would exhibit distortion in the crossover range for  $-V_{\gamma} < v_I < V_{\gamma}$  as is illustrated by curve a in Fig. 3. The distortion in the waveform is called crossover distortion or center clipping.

For  $V_B > 0$ , a positive bias voltage is applied to the base of  $Q_1$  and a negative bias voltage is applied to the base of  $Q_2$ . As  $V_B$  is increased, both transistors turn on and emitter currents flow that are given by

$$I_{E1} = I_{E2} = \frac{2V_B - V_{BE1} - V_{BE2}}{R_{E1} + R_{E2}}$$

The bias voltage causes the portion of curve a in Fig. 2 for  $v_I > 0$  to be shifted to the left and the portion for  $v_I < 0$  to be shifted to the right. The effective sum curve changes into approximately a straight line as shown in curve b in Fig. 2. This eliminates the crossover distortion in the output waveform in shown by curve b in Fig. 3.

Once the transistors are turned on, the emitter currents are extremely sensitive to the value of  $V_B$ . To reduce this sensitivity, resistors are often used in series with the emitters as shown in Fig. 1. If an excessive emitter current flows, the voltage drops across  $R_{E1}$  and  $R_{E2}$  cause  $V_{BE1}$  and  $V_{EB2}$  to decrease, causing the current to decrease. For minimum power dissipation in these resistors, their value must be much smaller than that of  $R_L$ . In the design of op amps, the emitter resistors are usually omitted. In this case, the value



Figure 2: Plots of  $v_O$  versus  $v_I$ . Curve a -  $V_B = 0$ . Curve b -  $V_B$  adjusted to eliminate the deadband region.



Figure 3: Sine wave (a) with and (b) without crossover distortion.

of  $V_B$  is chosen to bias the transistors just below cutoff. Although a small amount of crossover remains, it is minimized by the negative feedback that is used in the application of the op amps.

The circuit that is commonly used to bias a common-collector stage is the  $V_{BE}$  multiplier. Fig. 4 shows a simple  $V_{BE}$  multiplier consisting of transistor  $Q_3$  connected between the bases of  $Q_1$  and  $Q_2$ . The voltage across the multiplier is given by

$$V_B = I_1 R_1 + V_{BE3}$$

If the base current in  $Q_3$  is small compared to  $I_1$ , we can write  $I_1 = V_{BE3}/R_2$ . When this is substituted into the equation for  $V_B$ , we obtain

$$V_B = \frac{V_{BE3}}{R_2} R_1 + V_{BE3} = V_{BE3} \left( 1 + \frac{R_1}{R_2} \right)$$

It follows that the voltage  $V_B$  can be set by proper choice of the ratio  $R_1/R_2$ .



Figure 4: Complementary common-collector amplifier with a  $V_{BE}$  multiplier bias circuit.

The exact equation for  $V_B$  can be obtained by writing a node equation at the base node of  $Q_3$ . The equation is

$$\frac{V_B - V_{BE}}{R_1} = \frac{V_{BE}}{R_2} + \frac{1}{\beta} \left( I - \frac{V_B - V_{BE}}{R_1} \right)$$

This can be solved for  $V_B$  to obtain

$$V_B = V_{BE} \left( \alpha + \frac{R_1}{R_2} \right) + \frac{IR_1}{1+\beta}$$

where  $\alpha = \beta/(1+\beta)$  has been used. This agrees with the approximate solution above if  $\beta$  is large and  $IR_1 \ll 1+\beta$ .