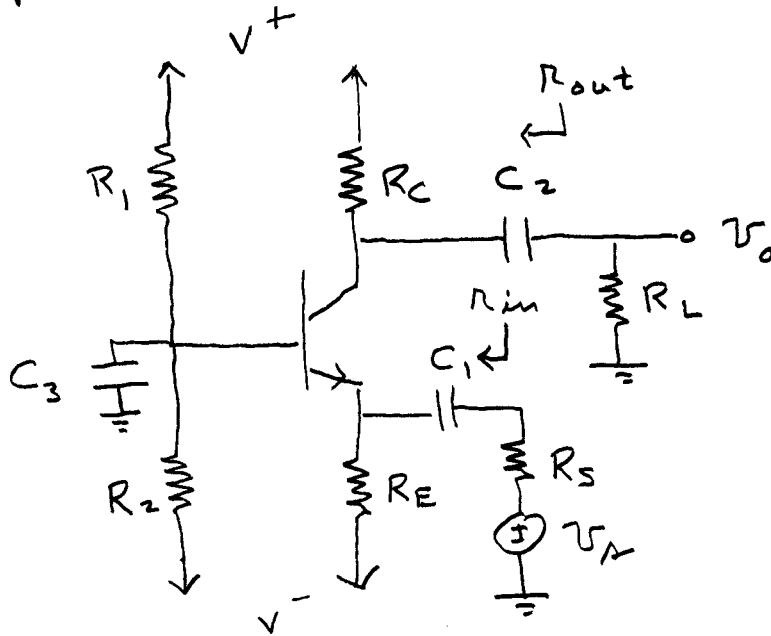


1-06/02/03

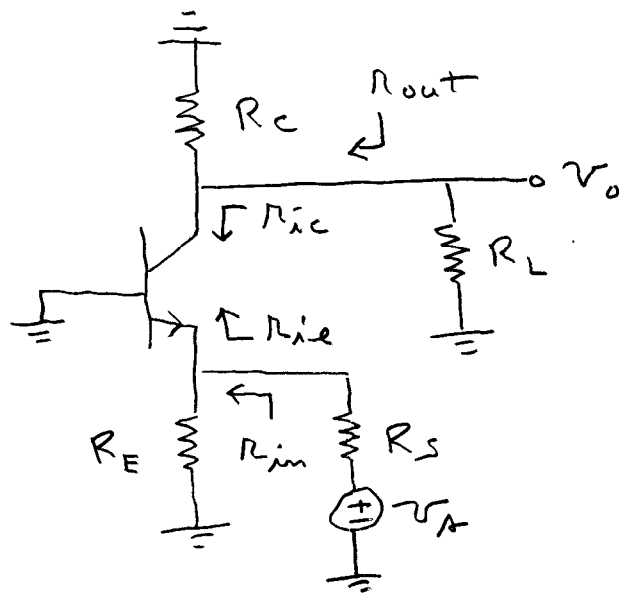
The Common Base (CB) Amplifier

For the CB amplifier, the signal is applied to the emitter and the output is taken from the collector. A typical capacitively coupled CB amplifier is shown.



The dc bias currents and voltages are solved for in the same way as for the CE amplifier. For the ac small-signal solution, set $v^+ = v^-$ and assume the capacitors are ac short circuits. The circuit reduces to,

2-06/02/03



The input and output resistances are given by

$$R_{in} = R_E \parallel R_{ie}$$

$$R_{out} = R_C \parallel R_{ic}$$

where

$$R_{ie} = r_e' \frac{r_o + R_{tc}}{r_e' + r_o + R_{tc} / (1 + \beta)}$$

$$R_{tc} = R_C \parallel R_L \quad R_{te} = R_E \parallel R_S$$

$$R_{ic} = \frac{r_o + r_e' \parallel R_{te}}{1 - \frac{\alpha R_{te}}{r_e' + R_{te}}}$$

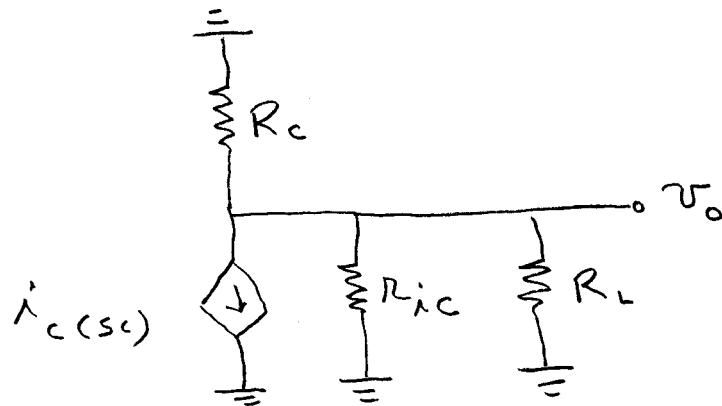
$$r_e' = \frac{R_{tb} + r_x}{1 + \beta} + r_e \quad R_{tb} = 0$$

3-06/02/03

Looking out of the emitter, the Thévenin equivalent circuit has the values

$$V_{te} = V_A \frac{R_E}{R_S + R_E} \quad R_{te} = R_E \parallel R_S$$

To solve for v_o , we replace the BJT with the Norton collector circuit,



$i_{c(sc)}$ is given by

$$\hat{i}_{c(sc)} = -G_{me} v_{te}$$

Where

$$G_{me} = \frac{1}{R_{te} + R'_e \parallel R_o} \quad \frac{\alpha R_o + R'_e}{R_o + R'_e}$$

4-06/02/03

The output voltage is given by

$$\begin{aligned}v_o &= -\hat{i}_{c(sc)} R_{ic} \parallel R_c \parallel R_L \\&= +G_{me} v_{te} R_{ic} \parallel R_c \parallel R_L \\&= +G_{me} v_{\pi} \frac{R_E}{R_s + R_E} R_{ic} \parallel R_c \parallel R_L\end{aligned}$$

Thus the voltage gain is given by

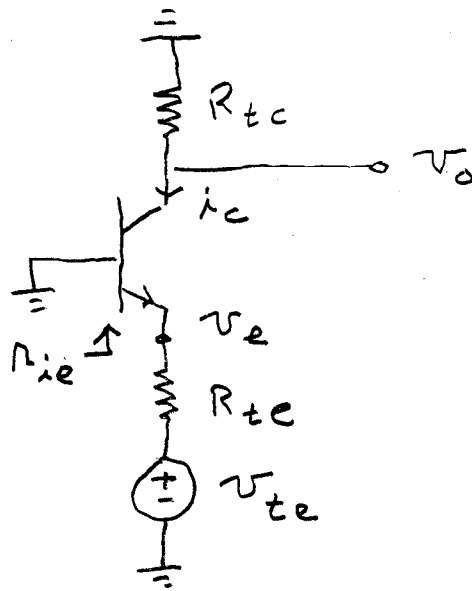
$$\begin{aligned}A_v &= \frac{v_o}{v_{\pi}} \\&= + \frac{R_E}{R_s + R_E} G_{me} R_{ic} \parallel R_c \parallel R_L\end{aligned}$$

The above solution is exact. Often, an approximate solution is made for rough calculations. Assume that $R_x = 0$ and $R_o = \infty$ for the approximations. In this case

$$\begin{aligned}R_{ie}' &= R_e' \\i_c &= \alpha i_e = g_m v_{be} = g_m (v_b^o - v_e) \\&= -g_m v_e\end{aligned}$$

5-06/02/03

The signal equivalent circuit is



$$v_e = v_{te} \frac{r_{ie}}{R_{te} + r_{ie}}$$

$$i_c = -g_m v_e$$

$$v_o = -i_c R_c = +g_m v_e R_{tc}$$

$$= +g_m v_{te} \frac{r_{ie}}{R_{te} + r_{ie}} R_{tc}$$

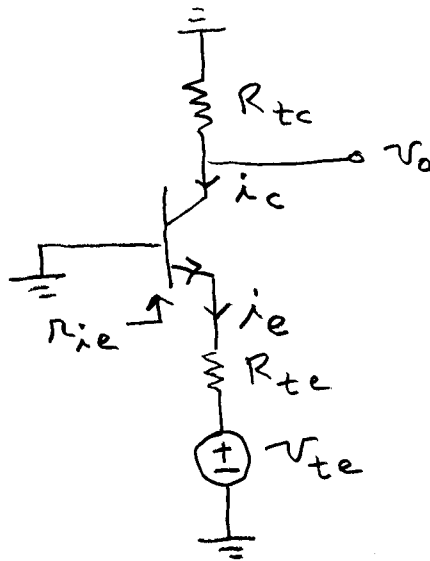
$$= +v_A \frac{R_E}{R_S + R_E} \frac{r_{ie}}{R_{te} + r_{ie}} g_m R_{tc}$$

$$\Rightarrow A_v = \frac{v_o}{v_A}$$

$$= \frac{R_E}{R_S + R_E} \frac{r_{ie}}{R_{te} + r_{ie}} g_m R_{tc}$$

6-06/02/03

An Alternate Approximate Solution



For $R_x = 0$ and $R_o = \infty$, r_{ie} is given by

$$r_{ie} = \frac{R_{tb}}{1+\beta} + r_e' = r_e' \quad (R_{tb} = 0)$$

$$i_e = - \frac{v_{te}}{R_{te} + r_e'}$$

$$i_c = \alpha i_e = -v_{te} \frac{\alpha}{R_{te} + r_e'}$$

$$v_o = -i_c R_{tc} = +v_{te} \frac{\alpha R_{tc}}{R_{te} + r_e'}$$

$$= +v_A \frac{R_E}{R_S + R_E} \frac{\alpha R_{tc}}{R_{te} + r_e'}$$

$$\Rightarrow A_v = \frac{v_o}{v_A} = + \frac{R_E}{R_S + R_E} \frac{\alpha R_{tc}}{R_{te} + r_e'}$$