EXAMINATION NO. 1 – SOLUTIONS (Average score = 60/100)

Problem 1 - (25 points)

Find an algebraic expression for the voltage gain, v_{out}/v_{in} , and the output resistance, R_{out} , of the source follower shown in terms of the small-signal model parameters, g_m and R_L (ignore r_{ds}). If the bias current is 1mA find the numerical value of the voltage gain and the output resistance. Assume that $K_N' = 110\mu A/V^2$, $V_{TN} = 0.7V$, and $K_P' = 50\mu A/V^2$, $V_{TP} = -0.7V$.

<u>Solution</u>

A small-signal model for this circuit is shown below neglecting r_{ds} of the transistors.





Summing currents at the output node gives,

$$g_{m1}v_{gs1} = g_{m3}v_{gs3} + G_Lv_{out}$$

Also, $v_{gs3} = -g_{m1}v_{gs1}(1/g_{m2})$
 $\therefore \quad g_{m1}v_{gs1} = g_{m3}\left(-\frac{g_{m1}}{g_{m2}}\right)v_{gs1} + G_Lv_{out}$
 $g_{m1}v_{gs1}\left(1 + \frac{g_{m3}}{g_{m2}}\right) = G_Lv_{out} \rightarrow$

Setting $v_{in} = 0$ and applying i_t and solving for v_{out} and ignoring R_L gives,

$$i_{t} = g_{m3}v_{gs3} + g_{m1}v_{out} = g_{m3}\left(\frac{g_{m1}}{g_{m2}}\right)v_{out} + g_{m1}v_{out}$$

$$\therefore \quad \frac{v_{out}}{i_{t}} = \boxed{R_{out} = \frac{1}{g_{m1}\left(1 + \frac{g_{m3}}{g_{m2}}\right)}}$$

Note that the 1mA splits between M1(M2) and M3 in a ratio of 1 to 100. Therefore, $I_{D1} = I_{D2} = 9.9 \mu A$ and $I_{D3} = 990.1 \mu A$.

$$\therefore g_{m1} = \sqrt{2 \cdot 110 \cdot 100 \cdot 9.9} = 466.71 \mu \text{S}, g_{m2} = \sqrt{2 \cdot 50 \cdot 1 \cdot 9.9} = 31.47 \mu \text{S}$$

and $g_{m3} = \sqrt{2 \cdot 110 \cdot 100 \cdot 990.1} = 3146.7 \mu \text{S}$

$$\frac{v_{out}}{v_{in}} = \frac{466.71 \cdot 101}{466.71 \cdot 101 + 1/50} = \frac{47.137}{47.137 + 20} = \underline{0.702 \text{ V/V}}$$
$$R_{out} = \frac{1000}{47.137} = \underline{21.2\Omega}$$

Problem 2 - (25 points)

Using the open-circuit and short-circuit time constant methods, find the two poles of the circuit shown below (assuming that the two poles are far apart from each other). $\beta_0=100$, $I_c=0.5$ mA, $f_T=1$ GHz, $C_{\mu}=0.2$ pF, $V_T=26$ mV.



<u>Solution</u>

$$r_{\pi} = \beta_0 / g_m = 100 \times 26 / 0.5 = 5.2 k \Omega$$

 $\tau_T = 1/(2\pi f_T) = 159 ps$

 $C_{\pi} = g_m \tau_T - C_u = (0.5/26) \times 159 pF - 0.2 pF = 2.86 pF$

$$R_I = R_I || r_{\pi} = 1.04 k \Omega$$

Open circuit time constant method:

$$P_1 \approx 1/\Sigma \tau = [R_1 C_{\pi} + (R_1 + R_L + g_m R_1 R_1) C_{\mu}]^{-1} = 22.13 \times 10^6 rad/s = 3.52 MHz$$

Short circuit time constant method:

 $P_2 \cong \Sigma(1/\tau) = [(R_1 || 1/g_m || R_L) C_{\pi}]^{-1} + [R_L C_{\mu}]^{-1} = 7.224 \times 10^9 rad/s = 1.15 GHz$

Problem 3 - (25 points)

a) For the emitter follower output stage shown below, find the value of R_1 for maximum efficiency and find the value of that efficiency. $V_{CC} = -V_{EE} = 2.5$ V, $V_{CE}(sat) = 0.2$ V, $R_L = 10$ k Ω , $V_{BE}(on) = 0.7$ V.

b) A load capacitor of 100pF is attached to the output voltage. If the input voltage suddenly drops from 2.5V to -2.5V, explain what happens at the output and accurately sketch the output voltage as a function of time, specifying its initial and final values and times.

<u>Solution</u>

The I_O for maximum efficiency is found as,

$$I_{Q} = \left(\frac{V_{CC} - V_{CE}(sat)}{R_{L}}\right) = 230\mu\text{A}$$

$$R_{I} = \left(\frac{-V_{EE} - V_{BE}}{I_{Q}}\right) = 7.826\text{k}\Omega$$

$$P_{L}(\max) = \left(\frac{V_{CC} - V_{CE}(sat)}{\sqrt{2}}\right) \left(\frac{I_{Q}}{\sqrt{2}}\right) = 0.5(2.3\text{V})(0.23\text{mA}) = 0.2645\text{mW}$$

$$P_{supply} = 2V_{CC}I_{Q} = 2(2.5)(0.23\text{mA}) = 1.15\text{mW}$$

$$\eta = \frac{P_{L(\max)}}{P_{\sup ply}} = \frac{1}{4} \left(1 - \frac{V_{CE}(sat)}{V_{CC}}\right) = 23\%$$

b) The output would slew under such condition. The current will be limited by the bias current:

Slew rate=0.23mA/100pF=2.3V/µs



Problem 4 - (25 points)

Find the numerical values of all roots and the midband gain of the transfer function v_{out}/v_{in} of the differential amplifier shown. Assume that $K_N' = 110\mu A/V^2$, $V_{TN} = 0.7V$, and $\lambda_N = 0.04V^{-1}$. The values of $C_{gs} = 0.2$ pF and $C_{gd} = 20$ fF.

<u>Solution</u>

A small-signal model appropriate for this circuit is shown.





Summing the currents at the output nodes gives,

$$g_{m1}v_{gs1} + sC_{gd}(v_{out} - v_{in}) + (g_{ds1} + G_L)v_{out} + sC_L v_{out} = 0$$

(Note: we are ignoring the fact that v_{out} and v_{in} should be divided by two since it makes no difference in the results and is easier to write.) Replacing v_{gs1} by v_{in} gives

$$-(g_{m1} - sC_{gd})v_{in} = [(g_{ds1} + G_L) + sC_L + sC_{gd}]v_{out}$$
$$\frac{v_{out}}{v_{in}} = \frac{-(g_{m1} - sC_{gd})}{s(C_L + C_{gd}) + (g_{ds1} + G_L)} = \left(\frac{-g_{m1}}{g_{ds1} + G_L}\right) \left(\frac{1 - \frac{sC_{gd}}{g_m}}{1 + s\frac{C_L + C_{gd}}{g_{ds1} + G_L}}\right)$$

:. MGB =
$$-g_{m1}(r_{ds}||R_L)$$
, Zero = $\frac{g_m}{C_{gd}}$ and Pole = $-\frac{g_{ds} + G_L}{C_{gd} + C_L}$
 $g_m = \sqrt{2.110.100.500} = 3316.7\mu$ S and $r_{ds} = \frac{1}{\lambda I_D} = \frac{25}{500\mu A} = 50 \text{ k}\Omega$

$$\therefore \quad \text{MGB} = -3.3167 \text{mS} \cdot (10 \text{k}\Omega \| 50 \text{k}\Omega) = \underline{-27.64 \text{ V/V}}$$

$$Zero = \frac{3.3167 \times 10^{-3}}{20 \times 10^{-15}} = \underline{1.658 \times 10^{11} \text{ radians/sec.}}$$
$$Pole = \frac{-1}{1.02 \times 10^{-12} (10 \text{k}\Omega \parallel 50 \text{k}\Omega)} = \underline{-1.1176 \times 10^8 \text{ radians/sec.}}$$