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# GEORGIA INSTITUTE OF TECHNOLOGY School of Electrical and Computer Engineering 

ECE 4430
Fall 2002

Third Exam

November 27, 2002

General Instructions:

1. Write on one side of the paper. (1 Pt.)
2. Put answers to all questions in the spaces provided on the test. (1 Pt.)
3. Show all work for full credit on questions requiring calculations. No credit will be given for answers alone, without supporting work.
4. Problems and questions are weighted as indicated. The maximum score is 100 points.
5. If you need more paper (provided in class), remove the staple from the exam and, when finished, arrange the test in order. Place the extra pages with supporting work in the test behind the page where the problem appears and indicate accordingly. Staple the entire test together so that there are no loose pages. (1 Pt.)

TEST SCORE: $\qquad$ / 100

I certify that I have neither given nor received any assistance while taking this test from anyone. (Signature) (1 Pt.)
$\square$ Place a check mark in the box if you observed any suspicious actions while taking this test.

Formula Sheet: Equations/Constants that you may, or may not, need are listed below:
$\mathrm{K}^{\prime}=50 \mu \mathrm{~A} / \mathrm{V}^{2}$ (unless otherwise stated in the problem)
$\mathrm{K}_{\mathrm{n}}=\mathrm{K}^{\prime} \mathrm{W} / \mathrm{L}$
$\lambda=0.01 \mathrm{~V}^{-1}$ (unless otherwise stated in the problem)
$\mathrm{V}_{\mathrm{TO}}=0.7 \mathrm{~V}$ (unless otherwise stated in the problem)
$\gamma=0.5 \mathrm{~V}^{1 / 2}$ (unless otherwise stated in the problem)
$2 \varphi_{\mathrm{F}}=0.6 \mathrm{~V}$ (unless otherwise stated in the problem)
$\mathrm{I}_{\mathrm{D} \text {-Triode }}=\left(\mathrm{K}_{\mathrm{n}} / 2\right)\left[2\left(\mathrm{~V}_{\mathrm{GS}}-\mathrm{V}_{\mathrm{TN}}\right) \mathrm{V}_{\mathrm{DS}}-\mathrm{V}_{\mathrm{DS}}{ }^{2}\right]$
$\mathrm{I}_{\mathrm{D}-\mathrm{Sat}}=\left(\mathrm{K}_{\mathrm{n}} / 2\right)\left(\mathrm{V}_{\mathrm{GS}}-\mathrm{V}_{\mathrm{TN}}\right)^{2}\left(1+\lambda \mathrm{V}_{\mathrm{DS}}\right)$
$\mathrm{V}_{\mathrm{TN}}=\mathrm{V}_{\mathrm{TO}}+\gamma\left[\operatorname{sqrt}\left(2 \varphi_{\mathrm{F}}-\mathrm{V}_{\mathrm{BS}}\right)-\operatorname{sqrt}\left(2 \varphi_{\mathrm{F}}\right)\right]$
$\mathrm{r}_{\mathrm{o}-\mathrm{MOS}} \approx 1 /\left(\lambda \mathrm{I}_{\mathrm{DS}}\right)$
$\mathrm{g}_{\mathrm{m}-\mathrm{MOS}}=\operatorname{sqrt}\left[2 \mathrm{I}_{\mathrm{DS}} \mathrm{K}_{\mathrm{n}}\right]$
$\mathrm{V}_{\mathrm{d} \text {-sat }}=\operatorname{sqrt}\left(2 \mathrm{I}_{\mathrm{DS}} / \mathrm{K}_{\mathrm{n}}\right)$
$\mathrm{g}_{\mathrm{mb}-\mathrm{MOS}}=\eta \mathrm{g}_{\mathrm{m}-\mathrm{MOS}}$
$\eta=\gamma \div 2 \operatorname{sqrt}\left(2 \varphi_{\mathrm{F}}-\mathrm{V}_{\mathrm{BS}}\right)$
$\mathrm{V}_{\mathrm{t}}=\mathrm{kT} / \mathrm{q} \approx 26 \mathrm{mV}$ and $\mathrm{I}_{\mathrm{S}}=1 \mathrm{E}-15 \mathrm{~A}$ (unless otherwise stated in the problem)
$\mathrm{I}_{\text {Diode }}=\mathrm{I}_{\mathrm{S}}\left[\exp \left(\mathrm{V}_{\mathrm{D}} / \mathrm{V}_{\mathrm{t}}\right)-1\right]$
$\mathrm{C}_{\mathrm{j}}=\frac{\mathrm{C}_{\mathrm{j} 0}}{\left(1-\frac{\mathrm{vD}_{\mathrm{D}}}{\psi_{\mathrm{o}}}\right)^{\mathrm{m}}} \quad \rightarrow 0.33 \leq \mathrm{m} \leq 0.5$
$\mathrm{V}_{\mathrm{A}}=100 \mathrm{~V}$ (unless otherwise stated in the problem)
$\beta_{\mathrm{F}}=50$ (unless otherwise stated in the problem)
$\mathrm{I}_{\mathrm{CE}}=\mathrm{I}_{\mathrm{S}}\left[\exp \left(\mathrm{V}_{\mathrm{BE}} / \mathrm{V}_{\mathrm{t}}\right)-1\right]\left[1+\mathrm{V}_{\mathrm{CE}} / \mathrm{V}_{\mathrm{A}}\right]$
$\mathrm{r}_{0-\mathrm{NPN}}=\mathrm{V}_{\mathrm{A}} / \mathrm{I}_{\mathrm{CE}}$
$\mathrm{g}_{\mathrm{m}-\mathrm{NPN}}=\mathrm{I}_{\mathrm{CE}} / \mathrm{V}_{\mathrm{t}}$
$\mathrm{CMRR}=\left|\mathrm{A}_{\mathrm{dm}}\right| /\left|\mathrm{A}_{\mathrm{cm}}\right|$
$\mathrm{Z}_{\text {miller-in }}=\mathrm{Z} /(1-\mathrm{k})$
$\mathrm{Z}_{\text {miller-out }}=\mathrm{Zk} /(\mathrm{k}-1)$

## Current Source/Sink Mirrors - Part A (34 Points)

1. An ideal current mirror has high / low output resistance.
2. An ideal current mirror has high / low input resistance.
3. Using the figure shown below and assuming that the collector-emitter resistance ( $\mathrm{r}_{\mathrm{o}}$ ) of bipolar transistors is equivalent to the largest possible drain-source resistance $\left(r_{d s}\right)$ of MOS devices $\left(r_{\mathrm{o}_{-} \text {ce }} \approx\right.$ $\left.\mathrm{r}_{\mathrm{ds} \_\max } \rightarrow \mathrm{V}_{\mathrm{A}} \approx 1 / \lambda_{\min }\right)$ and the overdrive $\left(\mathrm{V}_{\mathrm{DS} \_ \text {sat }}\right)$ of all MOSFETs is roughly 0.3 V , answer the following questions.

a) Why was MNA added to Circuit A?
b) What is the purpose of MNC and the resistor in Circuit C?
c) What is the purpose of MND in Circuit D?

d) Which circuit has the lowest output $\mathrm{V}_{\text {min }}$ (lowest output voltage possible for which the circuit still operates properly)?
e) Which circuit mirrors the current most accurately ( $\mathrm{I}_{\mathrm{in}}=\mathrm{I}_{\text {out }}$-no systematic errors- $)$ and why?
f) Which circuit has the worst accuracy (with respect to systematic errors only) and why?
4. Derive the output resistance $\left(\mathrm{R}_{\text {out }}\right)$ of the circuit illustrated below as a function of small-signal parameters $r_{\mathrm{o} 1}, \mathrm{r}_{\pi 1}, \mathrm{~g}_{\mathrm{m} 1}, \mathrm{r}_{\mathrm{ds} 2}, \mathrm{~g}_{\mathrm{m} 2}, \mathrm{r}_{\mathrm{ds} 3}, \mathrm{~g}_{\mathrm{m} 3}, \mathrm{r}_{\mathrm{ds} 4}, \mathrm{~g}_{\mathrm{m} 4}$, etc., and assume $\beta$ is infinite for the NPN transistor.


## Differential Amplifiers - Part B (48 Points)

Using the folded-cascode amplifier circuit shown, answer the following questions.

1. What is the purpose of QNB?
2. What is the purpose of MNB11?
3. What is the value of DC current $\mathrm{I}_{\mathrm{EE}}$ ?
(4 pts)

4. What is the value of DC current $\mathrm{I}_{12}$ ?
(assume $\beta_{\text {NPN }}$ is very large)
5. What is the value of DC current $\mathrm{I}_{21}$ ?
(assume $\beta_{\text {NPN }}$ is very large)
6. What is the value of DC voltage $\mathrm{V}_{\mathrm{B} 2}\left(\mathrm{~V}_{\mathrm{TP}}=1\right.$ and $\left.\mathrm{k}^{\prime}{ }_{P}=20 \mu \mathrm{~A} / \mathrm{V}^{2}\right)$ ?
7. What is the input common-mode voltage range (ICMR) of this
circuit, as a function of constants and $\mathrm{V}_{\mathrm{BE}}, \mathrm{V}_{\mathrm{T}}, \mathrm{V}_{\mathrm{DS} \text { _sat }}$, and $\mathrm{V}_{\mathrm{CE} \text { _min }}$ ?

$\leq \mathrm{V}_{\mathrm{icm}} \leq$
8. What is the maximum output voltage swing of this circuit (output common-mode range OCMR), as a function of constants and $\mathrm{V}_{\mathrm{T}}, \mathrm{V}_{\mathrm{DS} \text { _sat }}$, and $\mathrm{V}_{\mathrm{CE} \text { _min }}$ ?
9. Derive the differential gain to $\mathrm{v}_{12}$ (i.e., $\mathrm{v}_{12} / \mathrm{v}_{\mathrm{id}}$ ), as a function of $g_{m}, r_{d s}, r_{0}, r_{\pi}$, etc.? (6 pts)

10. Derive the gain from $v_{12}$ to output $v_{\text {out }}\left(\right.$ i.e., $\left.v_{\text {out }} / v_{12}\right)$, as a function of $g_{m}, r_{d s}, r_{0}, r_{\pi}$, etc.?

## References - Part C (14 Points)

1. An ideal voltage reference has high / low output resistance.
2. Ideally, the resistance between a voltage reference and the supply voltage is high / low.
3. Why does a bootstrapped reference require a start-up circuit?

4. Given base-emitter $\left(V_{\mathrm{BE}} \rightarrow \mathrm{V}_{\mathrm{ref}}=A V_{\mathrm{BE}}\right.$ or $\left.\mathrm{I}_{\mathrm{ref}}=\mathrm{V}_{\mathrm{BE}} / \mathrm{R}\right)$ and gate-source $\left(\mathrm{V}_{\mathrm{GS}} \rightarrow \mathrm{V}_{\mathrm{ref}}=A V_{\mathrm{GS}}\right.$ or $\mathrm{I}_{\mathrm{ref}}=$ $\mathrm{V}_{\mathrm{GS}} / \mathrm{R}$ ) voltage derived reference circuits, the base-emitter / gate-source derived reference circuits have lower sensitivity to the supply voltage. Explain your answer below.

## Part A.

1. High
2. Low
3.a. To eliminate base-current errors
3.b. To bias QN 2 with a low $\mathrm{V}_{\mathrm{CE}} \rightarrow$ To decrease the output $\mathrm{V}_{\text {min }}$ of the circuit
3.c. To increase the output resistance of the current mirror circuit
3.d. A
3.e. $\mathrm{B} \rightarrow$ There are no Early voltage errors $\left(\mathrm{V}_{\mathrm{CE} 1}=\mathrm{V}_{\mathrm{CE} 2}\right)$ and no base-current errors $\left(\mathrm{I}_{\mathrm{CN} 1}=\mathrm{I}_{\mathrm{in}}\right)$
3.f. $C \rightarrow$ Base-current errors exist as well as Early voltage effects $\left(V_{C E 1} \neq V_{C E 2}\right)$
3. $R_{\text {out }}=\left(I_{t}-g_{m 2} V_{g s 2}\right) r_{d s 2} / I_{t}=\left(I_{t}-g_{m 2}\left[V_{g}-V_{s}\right]\right) r_{d s 2} / I_{t}$

$$
\begin{gathered}
\mathrm{v}_{\mathrm{g}}-\mathrm{v}_{\mathrm{s}}=-\mathrm{v}_{\mathrm{s}}\left(\mathrm{~g}_{\mathrm{m} 3} \mathrm{r}_{\mathrm{d} s}+1\right)=-\mathrm{I}_{\mathrm{t}} \mathrm{r}_{\mathrm{o} \_\mathrm{ce}}\left(\mathrm{~g}_{\mathrm{m} 3} \mathrm{r}_{\mathrm{ds} 3}+1\right) \\
\rightarrow \quad \mathrm{R}_{\mathrm{out}}=\left(\mathrm{I}_{\mathrm{t}}+\mathrm{g}_{\mathrm{m} 2}\left[\mathrm{I}_{\mathrm{t}} \mathrm{r}_{\mathrm{o}_{-} \mathrm{ce}}\left(\mathrm{~g}_{\mathrm{m} 3} \mathrm{r}_{\mathrm{ds} 3}+1\right)\right]\right) \mathrm{r}_{\mathrm{ds} 2} / \mathrm{I}_{\mathrm{t}} \\
=\left[1+\mathrm{g}_{\mathrm{m} 2 \mathrm{r}_{\mathrm{o}} \mathrm{ce}}\left(\mathrm{~g}_{\mathrm{m} 3} \mathrm{r}_{\mathrm{d} 3}+1\right)\right] \mathrm{r}_{\mathrm{ds} 2}
\end{gathered}
$$



## Part B.

1. To reduce base-current errors in the QNB1, QNB11, QNB2 current mirror
2. To increase the output resistance of current sink MNB11, QNB11
3. $\mathrm{I}_{\mathrm{EE}}=\mathrm{I}_{\mathrm{C}_{-} \mathrm{QNB} 11}=\mathrm{I}_{\mathrm{C}_{-} \mathrm{QNB} 1} \approx 10 \mu \mathrm{~A}(\mathrm{QNB} 1, \mathrm{QNB} 11$ is a 1-to-1 current mirror)
4. $\mathrm{I}_{12}=1.5 \mathrm{I}_{\mathrm{D}_{-} \mathrm{MPB} 1}=15 \mu \mathrm{~A}$ (MPB1, MP12 is a 1-to- 1.5 current mirror)
5. $\mathrm{I}_{21}=\mathrm{I}_{12}-\mathrm{I}_{\mathrm{EE}} / 2=10 \mu \mathrm{~A}$
6. $\mathrm{V}_{\mathrm{B} 2}=\mathrm{V}_{\mathrm{DD}}-\mathrm{I}_{\mathrm{C}_{-} \mathrm{QNB} 2} \mathrm{R}_{\mathrm{PB} 2}-\mathrm{V}_{\mathrm{SG}} \mathrm{MPB} 2=10-(10 \mu)(10 \mathrm{k})-\mathrm{V}_{\mathrm{TP}}-\mathrm{V}_{\mathrm{ON}-\mathrm{MPB} 2}$

$$
=10-0.1-1-\sqrt{\frac{2 I}{K_{P}^{\prime}(W / L)}}=8.9-1=7.9 \mathrm{~V}
$$

7. $\mathrm{V}_{\mathrm{CE} \text { _QNB11 }}+\mathrm{V}_{\text {DS_MNB11 }}+\mathrm{V}_{\mathrm{BE} \text {-QN12 }} \leq \mathrm{V}_{\mathrm{icm}} \leq \mathrm{V}_{\mathrm{DD}}-\mathrm{V}_{\mathrm{SD} \text { _MP12 }}-\mathrm{V}_{\mathrm{CE}_{-} \mathrm{QN} 12}+\mathrm{V}_{\mathrm{BE} \text { _QN12 }}$ where $\mathrm{V}_{\mathrm{CE}_{\text {-QNB11 }}}=\mathrm{V}_{\mathrm{BE} \text { _QNB1 }}+\mathrm{V}_{\mathrm{BE} \text { _QNB }}$

$$
\mathrm{V}_{\mathrm{DS} \_ \text {sat }}+3 \mathrm{~V}_{\mathrm{BE}} \leq \mathrm{V}_{\mathrm{icm}} \leq 10-\mathrm{V}_{\mathrm{SD} \_ \text {sat }}-\mathrm{V}_{\mathrm{CE} \_\min }+\mathrm{V}_{\mathrm{BE}}
$$

8. $\mathrm{V}_{\mathrm{CE} \text { _QN22 }} \leq \mathrm{V}_{\mathrm{O}} \leq \mathrm{V}_{\mathrm{DD}}-\mathrm{V}_{\mathrm{SD} \text { _MP12 }}-\mathrm{V}_{\mathrm{SD} \text { _MP22 }} \quad$ where $\mathrm{V}_{\mathrm{SD} \_\mathrm{MP} 22} \approx \mathrm{I}_{\mathrm{C}_{-} \mathrm{QNB} 2} \mathrm{R}_{\mathrm{PB} 2}$

$$
\mathrm{V}_{\mathrm{CE}_{-} \min } \leq \mathrm{V}_{\mathrm{O}} \leq 10-\mathrm{I}_{\mathrm{C}_{-} \mathrm{QNB} 2} \mathrm{R}_{\mathrm{PB} 2}-\mathrm{V}_{\mathrm{SD} \_\min }=10-0.1-\mathrm{V}_{\mathrm{SD} \_\min }=8.9-\mathrm{V}_{\mathrm{SD} \_\min }
$$

9. Since the emitters of QN11 and QN12 are ac-ground with a differential input signal

$$
\begin{gathered}
\rightarrow \text { common-emitter gain configuration } \\
\mathrm{v}_{12}=\left(\mathrm{v}_{\mathrm{id}} / 2\right)\left(-\mathrm{g}_{\mathrm{m}_{-} \mathrm{QN} 12}\right)\left(\mathrm{r}_{\mathrm{o}_{\_} \mathrm{QN} 12} / / \mathrm{r}_{\mathrm{sd} \_\mathrm{MP} 12} / /\left[1 / \mathrm{g}_{\mathrm{m}_{-} \mathrm{MP} 22}\right]\right) \approx\left(\mathrm{v}_{\mathrm{id}} / 2\right)\left(-\mathrm{g}_{\mathrm{m}_{\_} \mathrm{QN} 12}\right)\left(1 / \mathrm{g}_{\mathrm{m}_{-} \mathrm{MP} 22}\right) \\
\mathrm{v}_{12} / \mathrm{v}_{\mathrm{id}}=-\mathrm{g}_{\mathrm{m}_{-} \mathrm{QN} 12} /\left(2 \mathrm{~g}_{\mathrm{m}_{-} \mathrm{MP} 22}\right)
\end{gathered}
$$

10. Common-gate gain configuration $\rightarrow \mathrm{v}_{\text {out }} \approx \mathrm{v}_{12} \mathrm{~g}_{\mathrm{m}_{\text {_MP22 }}} \mathrm{r}_{\mathrm{o}_{-} \mathrm{QN} 22}$ or $\quad \mathrm{v}_{\text {out }} / \mathrm{v}_{12} \approx \mathrm{~g}_{\mathrm{m} \_ \text {MP22 }} \mathrm{r}_{\mathrm{O}_{-} \mathrm{QN} 22}$ (the resistance seen into the drain of MP22 is assumed to be much larger than $\mathrm{r}_{\mathrm{o}_{\mathrm{O}} \mathrm{QN} 22}$-cascoded resistance $\rightarrow$ source-degenerated circuit-)

## Part C.

1. Low
2. High
3. Bootstrapped references have two or more possible states of operation (e.g., on and off states).

Consequently, a start-up circuit is necessary to ensure the circuit operates in the desired state.
4. Base-emitter $\rightarrow$ An exponentially larger change in current is required to alter $\mathrm{V}_{\mathrm{BE}}$ whereas

MOSFETs require a square-law change to alter $\mathrm{V}_{\mathrm{GS}} \rightarrow$ lower output resistance.

