EXAMINATION NO. 2 - SOLUTIONS (Average Score = 80/100)

Problem 1 - (25 points)

A frequency synthesizer is shown below and has the following parameters:

$$F(s) = \frac{1 + 0.01s}{s} \qquad K_o = 2x10^6 \text{ (rads/V)} \qquad K_d = 0.8 \text{ (V/rad.)}$$

$$\beta = 2\pi \qquad N = 150 \qquad f_{ref} = 120 \text{ kHz}$$

$$\theta_{ref} \xrightarrow{A} \qquad K_d \qquad f_{ref} \xrightarrow{F(s)} \xrightarrow{C} \qquad F(s) \qquad f_{ref} \xrightarrow{E} \qquad 0.5 \text{ (V/rad.)}$$

(a.) Where would you introduce the modulating voltage, v_p , if you wish to phase modulate the output of the synthesizer (*A*, *B*, *C*, *D*, *E*, or *F*)?

(b.) What is the peak amplitude of a 1kHz ac signal needed to produce an output peak phase deviation of 0.5 radians?

<u>Solution</u>

...

(a.) The modulating voltage should be introduced at *B*.

(b.) The transfer function between the input modulating voltage and the output phase is given as,

$$\begin{aligned} \theta_o(s) &= \frac{K_o}{s} F(s) \left[V_p(s) - K_d \frac{\theta_o}{N} \right] \quad \Rightarrow \quad \theta_o(s) \left[1 + \frac{K_o K_d F(s)}{sN} \right] = \frac{K_o F(s)}{s} V_p(s) \\ \frac{\theta_o(s)}{V_p(s)} &= \frac{K_o F(s)}{s + \frac{K_v F(s)}{N}} = \frac{K_o (1 + 0.01s)}{s^2 + \frac{0.01 K_v}{N} s + \frac{K_v}{N}} \\ \omega_n &= \sqrt{\frac{K_v}{N}} = \sqrt{\frac{1.6 \times 10^6}{150}} = 103 \text{ rads/sec. (16.4 Hz)} \text{ and } \zeta = \frac{K_v}{100N} \sqrt{\frac{N}{K_v}} \approx 1 \end{aligned}$$

Since, $f_n \ll 1$ kHz, the transfer function can be approximated as,

$$\left|\frac{\theta_o(j\omega)}{V_p(j\omega)}\right| \approx \frac{0.01K_o}{\omega} = \frac{20,000}{2000\pi} = 3.183$$

 $\therefore \text{ A phase deviation of } 0.5 \text{ radians requires a modulating voltage of } 0.5/3.183 \text{ or } 0.157\text{V}$ $\boxed{\text{Peak deviation of the modulating voltage} = 0.157\text{V}}$

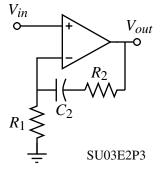
Problem 2 - (25 points)

(a.) Find the transfer function of the filter shown assuming an ideal op amp.

(b.) Sketch a Bode plot for the magnitude of this filter if $R_1 = R_2$

= $10k\Omega$ and $C_2 = 0.159\mu$ F.

(c.) For the values in part (b.), find the single sideband spur at a reference frequency of 25 kHz if the op amp has an input offset current of $I_{os} = 50$ nA and an input offset voltage of $V_{io} = 100$ µV. Assume that the spurious deviation due to the offset voltage at 25 kHz can be expressed as $\theta_d = 100V_{pm}$, where V_{pm} is the phase modulation caused by the offset voltage of the filter.



<u>Solution</u>

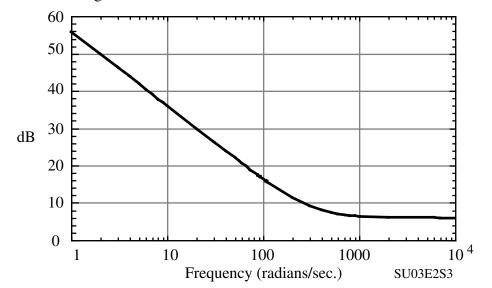
(a.) The transfer function assuming an ideal op amp can be found as,

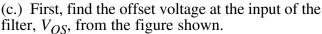
$$\frac{V_{out}(s)}{V_{in}(s)} = \frac{Z_1 + Z_2}{Z_1} = \frac{R_1 + R_2 + (1/sC_2)}{R_1} = \frac{s(R_1 + R_2)C_2 + 1}{sC_2R_1}$$

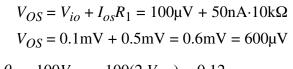
(b.) If $R_1 = R_2 = 10 \text{k}\Omega$ and $C_2 = 0.159 \mu\text{F}$, then the filter transfer function becomes,

$$F(s) = \frac{s(R_1 + R_2)C_2 + 1}{sC_2R_1} = \frac{s0.00318 + 1}{0.00159s} = \frac{\frac{3}{314.5} + 1}{\frac{s}{628.9}}$$

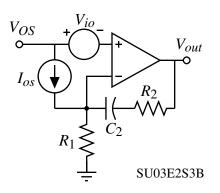
The sketch for the magnitude of this transfer function is below.







$$SSB = 20 \log_{10}(\theta_d/2) = -24.44 \text{ dBc}$$



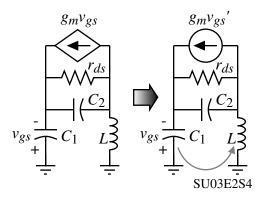
Problem 3 - (25 points)

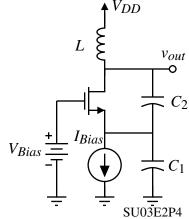
Find the oscillation frequency, ω_{osc} and the value of $g_m r_{ds}$ necessary to oscillate in terms of *L*, *C*₁, and *C*₂ for the *LC* oscillator shown.

<u>Solution</u>

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The small-signal model for solving this problem is shown below.





Note that the current from the independent source has two paths. One is through the parallel combination of r_{ds} and C_2 , and the other is through C_1 and L.

The open-loop gain, V_{gs} '/ V_{gs} can be found as,

At the oscillation frequency, we can write that,

$$-g_m r_{ds} = 1 - \omega_{osc}^2 L C_1 = 1 - \frac{C_1 + C_2}{C_2} = 1 - 1 - \frac{C_1}{C_2} = -\frac{C_1}{C_2}$$

$$\therefore \qquad g_m r_{ds} = \frac{C_1}{C_2}$$

Problem 4 – (25 points)

A model for single sideband noise using the time-invarient theory is given by

$$\mathcal{L}{f_m} = 10 \log \left\{ \frac{2FkT}{P_s} \left[1 + \frac{1}{4Q^2} \left(\frac{f_o}{f_m} \right)^2 \right] \left(1 + \frac{f_c}{f_m} \right) \right\}$$

(a.) Describe each term in this equation and give the units of the term.

(b.) If F = 2dB, what is the noise floor if the carrier power is 10 dBm at room temperature (27°C) and $k = 1.381 \times 10^{-23}$ Joules/K°?

(c.) Make an approximate sketch of $\mathcal{L}{f_m}$ in dBc as a function of $\log 10(f_m)$ and identify the various regions.

<u>Solution</u>

(a.)

F = the noise figure or factor depending upon terminology. It is unitless.

 $k = \text{Boltsmann's constant and is equal to } 1.381 \text{x} 10^{-23} \text{ Joules/K}^{\circ}.$

T = temperature in °K

 P_s = power in the carrier in watts.

Q =open-loop Q of the oscillator. It is unitless.

 f_o = carrier frequency in Hz.

 f_m = deviation frequency from the carrier in Hz.

 f_c = corner frequency in Hz associate where the 1/f noise is no longer significant.

(b.) The noise floor is 10 log $\left(\frac{2FkT}{P_s}\right)$. We need to perform some "preprocessing" first before using the equation.

$$F = 2 dB \rightarrow F = 10^{2/10} = 1.585 \text{ and } P_s = 10 dBm \rightarrow P_s = 10^{10/10} = 10 mW$$

 $\mathcal{L}{f_m} = 10 \log\left(\frac{2 \cdot 1.585 \cdot 1.381 \times 10^{-23} \cdot 300}{10 \times 10^{-3}}\right) = -178.8 dBc$

(c.)

 $\mathcal{L}[\Delta \omega]$ dBc/Hz

